

Stichtabstich

- (1) Cashmooor $\mu_{11} \leq \bar{K}_c \leq \mu_{11} + \Delta_{ct}$
- (2) Semi-discrete $\mu_{11} \leq \bar{K}_c \leq \mu_{11} + \Delta_{ct}$

Def: $\Delta \leq \Delta_0 + \sigma(\Delta)$ (3)

Wur schichtig starke

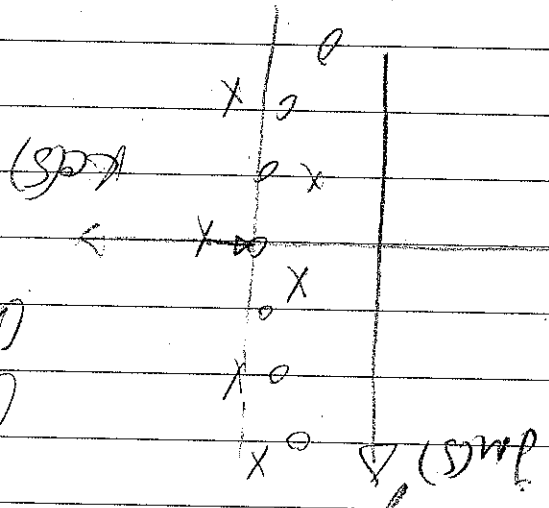
Note 1 Estimate for cont. case

must be sharp

Note 2 Maximum "grain" eigenvalue

must be captured.

(0) = cont
(x) = discrete



∴ Shrinkage Stress

$U_k = U_c = 1$ and $\Delta d = \Delta c = 0$

$q = 0 \Rightarrow \frac{11U_{11}}{2} \leq \frac{11U_{11}}{2}$ if $r < 50$

Energy $\Rightarrow (11U_{11})_t = U_0 (11r^2) - U_0 - 2U_0 q$

$U_{11} = f$
 $U_1 + \Delta U_1 = 0 = \rho \Delta U_0 q \dot{\epsilon}_0$

SRP & SMT

$q = 0 \Rightarrow \frac{11}{2} \leq \frac{11}{2}$ $f_c = q \cdot \Delta c = 0$

Energy $\Rightarrow 11U_{11} = 0q - U_{11}$

$U_{11} = q$
 $U_1 + \Delta U_1 = 0$
 $0 \leq X \leq 1$

Constant Coeff. (plate type 1)

3)

Variable Coeff (Probtype 2)

$$\begin{aligned}
 u + a(x)u_x &= 0 & u(0,1) &= 5 \\
 u(x,1) &= f & u(x,0) &= f \\
 a > 0 & & a > 0 &
 \end{aligned}$$

$$\alpha(u)_x + \beta a u_x + \gamma u_x = a u_x \Rightarrow$$

$$(\alpha + \beta) a u_x + (\alpha + \gamma) a u_x = a u_x$$

$$\alpha + \beta = 0 \quad \beta = -\alpha \quad \gamma = 1 - \alpha$$

$$u_x + \alpha(u)_x - \alpha a u_x + (1 - \alpha) a u_x = 0$$

$$\int (u_x + \alpha u_x) + \alpha \int (u_x)_x - \alpha \int a u_x + (1 - \alpha) \int a u_x dx = 0$$

$$\frac{1}{2} u^2 + \int a u_x - \alpha a u_x + (1 - \alpha) a u_x dx$$

$$\alpha \int a u_x dx =$$

(1)

Choose $-x + 1 - x = 0 \Rightarrow x = 1/2$

$$H(x) = \frac{1}{2} \frac{d^2 u}{dx^2} - \frac{1}{2} \frac{d^2 u}{dx^2} + \int_0^1 u dx =$$

$$= \frac{1}{2} \frac{d^2 u}{dx^2} - \frac{1}{2} \frac{d^2 u}{dx^2} + \int_0^1 u dx \quad (*)$$

Semidiscrete

$$U_1 + \frac{1}{2} P^T Q(AU) - \frac{1}{2} A^T U + \frac{1}{2} A^T P^T Q U =$$

$$P^T \alpha(U_0 - q) e_0$$

$$U(0) = 1$$

Energy \Rightarrow

$$U^T P^T Q U + \frac{1}{2} U^T A U + \frac{1}{2} U^T A^T Q U = U^T P^T A U$$

$$\frac{1}{2} U^T P^T A U - \frac{1}{2} (U^T A^T Q U) + \frac{1}{2} U^T A U$$

= 0

$$\frac{d}{dt} W(t) = \alpha_0 W(t) - \alpha_1 W(t) + U^T P W(t)$$

$$\approx \int_0^t \alpha dx$$

$$+ 2W(t)(W(t)-g) - (x)$$

$$BT W_0 (W_0 + 2x) - \alpha_1 W_0 - 2x W_0 g$$

$$\text{let } x = -W_0 \Rightarrow BT = \alpha_0 g - \alpha_1 W_0 - \alpha_1 (W_0 - g)$$

for comparison of (x) and (x*)

let $g=0$ and $\alpha_0 + 2x = 0 \Rightarrow$

$$(x) W(t) = -\alpha_1 W(t) + \int_0^t \alpha dx$$

$$\text{let } (W(t))' = -\alpha_1 W(t) + U^T P W(t)$$

(x*) Not necessarily strictly stable

Conservative Finite Difference Formulations, Variable Coefficients, Energy Estimates and Artificial Dissipation

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Artificial dissipation terms for finite difference approximations of linear hyperbolic problems with variable coefficients are determined such that an energy estimate and strict stability is obtained. Both conservative and non-conservative approximations are considered. The dissipation terms are computed such that there is no loss of accuracy.

KEY WORDS: Artificial dissipation; finite differences; stability; variable coefficients; energy estimate.

1. INTRODUCTION

Most difference methods for solving nonlinear hyperbolic problems are on conservative form. Conservation is required for a correct shock speed in a nonlinear problem, see [7]. For variable coefficient problems both conservative and non-conservative formulations are used. Examples of important variable coefficient problems include aeroacoustic (the linearized Euler equations), electro-magnetics (variable permittivity and permeability in the Maxwell's equations) and problems where curvilinear meshes with varying metric coefficients are used. Normally, the artificial dissipation is constructed to absorb the energy of unresolved modes in the problem. It can also be added to enable the calculation of problems involving shocks (see [9] for a discussion on artificial dissipation operators). In this paper we aim for a particular kind of

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